

SYNTHESIS REPORT
FOR PUBLICATION

Kopie

CONTRACT No.: BREU-CT91-0403

PROJECT No.: BE-4210

TITLE : SPUTTER COATINGS
ADJUSTMENT OF THE COATING DESIGN AND APPLICATION

PROJECT
COORDINATOR : HARTEC GES. FÜR HARTSTOFFE UND DÜNNSCHICHTTECHNIK
MBH & CO. KG

PARTNERS : GÜNTHER WIRTH - PRÄZISIONSWERKZEUGE

JAKOB BOSS SÖHNE KG

ECON INDUSTRIES, S.A.

FACULDADE DE CIENCIAS E TECNOLOGIA - UNI COIMBRA

ECOLE CENTRALE DE LYON

REFERENCE PERIOD FROM 01. SEPTEMBER 1991
TO 31. AUGUST 1995

PROLONGATION FROM 01. SEPTEMBER 1995
TO 31. DECEMBER 1995

STARTING DATE : 01. SEPTEMBER 1991 IKR?ITION: 52 MONTHS

PROJECT FUNDED BY THE EUROPEAN
COMMUNITY UNDER THE BRITE/EURAM
PROGRAMME

DATE : JUNE 1996

1. ABSTRACT

Sputter coatings are used industrially as hard coatings for protection of tools and tool devices **against wear** and corrosion'.

The most significant objectives **of this** project were the development of coatings based on new target materials and the optimization of the lifetime of cutting tools **by** means of **tool** design according to the properties of the new coatings.

Sintered targets with variable chemical composition based on tungsten alloyed with **titanium**, nickel, chromium and **other** metals were used to deposit thin films as nitrides, carbides and **carbonitrides**.

The study **of the** deposition conditions was carried out initially in a laboratory equipment. This work lead to the construction of a prototype with similar characteristics to a high rate sputtering system.

Thin films were deposited over high speed **steel** and cemented carbide cutting tools with standard and later with optimized geometries. The deposition conditions in the " prototype **were optimized** for grinded (cutting tools) and polished (samples)" surfaces, establishing the standard process parameters.

Samples coated with **GOLD-TiN**, **SILVER-TiN** and TiCN were supplied by means of industrial production of standard **coatings** deposited from a titanium target. The study of the coating Properties. was carried out in view of the optimization of the target chemical composition. Each target alloy was used to 'produce **coatings** for **cutting** tools to achieve higher lifetime and an optimal wear behaviour during service.

Comparative studies were carried out on a Fin-on-disc equipment, establishing the relationship between the wear rate and the friction coefficient of the sputtered coatings. **The** study of the wear **behaviour** was carried out at **room** temperature, as well as at temperatures up to 500 degrees Celsius for high speed steel coated samples and up to 600 degrees Celsius for cemented carbide coated samples.

A fretting test equipment was used to **complete** the study of the wear behaviour of the coatings at room temperature.

The wear behaviour of the new developed **coatings** was studied under real cutting conditions using coated high **speed** steel taps and thread formers and cemented carbide **mills** and **drills**. According to the properties of the optimized coatings, new tool geometries were developed. Finally, the cutting conditions **were optimized** for the tools with new geometries.

2. INTRODUCTION

The aim of the project was to develop new coated cutting **tools** with better cutting performances than those **obtained** by conventional coatings and tool geometries. Two important objectives should be reached, concerning the deposition of W-C-/N-Me (**Me=Metal**) coatings and the adjustment of the tool geometries to the properties of the new developed coatings.

The definition of the target chemical **composition**, which leads to the optimal film properties, as high hardness and tenacity, high temperature and abrasive wear resistance, **low** friction coefficient and high deposition rate, was certainly **the most important** subject 'to be **analysed**.

A first study on the deposition conditions was carried out in a laboratory 'equipment, where different **target** materials were used, establishing simultaneously the basic work for the definition of a **PVD** coating equipment with characteristics **similar** to "an industrial system; The conception of the sputtering system' included a planar magnetron cathode, an ion beam source positioned in front **of** that cathode and a rotational substrate holder. This system allows the' coating deposition using simultaneously the ion beam source to increase the plasma ionisation.

The **vacuum** equipment with an ultimate pressure under 10^{-6} **mbar** works at pressure values **under** 3×10^{-3} mbar and at deposition rates up to $0,35 \mu\text{m}/\text{min}$. in order to guarantee the purity, Of the coating chemical composition and the rentability of **the** deposition **process**.

The application of coatings to" cutting **tools** leads generally to severe alterations of the cutting conditions. For adjusting these conditions to achieve the best results, it was necessary to acquire complete' basic data for standard tools coated under standard conditions and establish the relationships between the coating properties and the cutting conditions **and** the tool geometries depending on the tool and worked materials:

Standard tool geometries were used to optimize the pre-heating, etching **and** deposition conditions in the prototype equipment and to study the influence of the coating properties and **film** thickness **on** tool **geometry** and on their cutting performances.

The correlation of the film properties **with** the wear phenomena was investigated, in order to develop new **cutting** tool geometries designed' for optimum surface treatment and manufacturing productivity. These tools **should** work at high cutting speed and feed rates, **also** without lubricant or coolant.

3. TECHNICAL DESCRIPTION

3.1. SELECTION OF THE BASE MATERIAL FOR THE COATING

The deposition conditions were initially optimized, when reactive sputtering from a pure tungsten target. The study of the influence of the elements nitrogen and carbon on the " properties of the **films** showed that the increase of **nitrogen** flow rate makes the film more. oriented in (110) direction and decreases the coating hardness, specially when the **W₂N** phase is **present**. Scratch-test results have shown that W-N films fail always cohesively, firstly by tensile cracking and after by chipping. The structure of W-C/N films is different, where the phase WC carbide was **detected**. This phase is **isomorphous** of **WN**.

In addition to the **element** tungsten, a preliminary selection of the metallic elements for the target material **was** carried out, using chromium, nickel and titanium to analyze the **influence** of the 'second metallic element. The study was carried out in non-reactive mode to compare the results with those of amorphous and crystalline W-C-Co.

The deposition of **W-C-Ni** coatings have shown that the addition of Ni leads to the **amorphization** of the **films** when its content in the film overcomes a **threshold** value of 5 % **atomic**. In this system was detected the presence of. "free" Ni. The crystallisation mechanisms were **observed** depending on the chemical **composition**: for Ni < 9 at% two phases **WC + W₂C** are formed and for higher Ni contents **an initial** precipitation of WC + Ni occurs.

In comparison to previous results obtained with the system **W-C-Co**, films deposited from **W-C-Cr**, **W-C-Ni** and **W-C-Ti** targets present adhesive failures and lower cohesive critical loads. The hardness of these **films** is lower than that of crystalline W-C-Co films and slightly higher than amorphous W-C-Co **films**. The adhesive critical load increases **with increasing** titanium **content** and with increasing negative substrate **bias**. Any influence of the chromium content "or of the substrate bias on the film properties cohesive and adhesive critical loads, as well as on the **microhardness**, could be found for **W-C-Cr** films.

The morphology of' the films sputtered from a pure tungsten target in a reactive atmosphere is more compact than that of the **W-Ti-N** films. No signs of nitrides could be detected in films of the W-N system, where nitrogen **was** found only in a **solid** solution. The reactivity of tungsten in the **plasma** environment is very low compared with that of titanium. **W-Ti-N** films present nitrides in their . structure at the same **nitrogen/argon** ratio levels as for the W-N system.

3.2. ADJUSTMENT OF THE DEPOSITION CONDITIONS OBTAINED IN THE LABORATORY **EQUIPMENT TO THE PROTOTYPE**

The concept for the prototype considered **some** special features:

- each sample to be treated can be rotated **with constant** speed
- the samples are preheated by means of **electron bombardement**
- **the sputter** cleaning process is **achieved very** easily by means of inversion of the substrate tension
- during the deposition of films it is possible to variate the distance between cathode **and** substrate
- the ion beam source can also contribute to **increase** the ionization **level**, when working simultaneously with the magnetron cathode. '

The deposition conditions were optimized concerning the "influence of the ultimate pressure on the coating properties and the influence of the **pre-heating** and ion etching parameters on the surface roughness and on the mechanical properties of the coatings.

The influence of the ultimate pressure on the coating properties was studied comparing the results of the **hardness** and scratch tests, obtained on films deposited after the deposition chamber have been evacuated during different times. The results show that both hardness and scratch" test critical loads increase with decreasing ultimate pressure. In order to achieve reasonable **results** and simultaneously to satisfy the industry requirement of low evacuation time, the deposition was carried out at an ultimate **pressure** of $7.5 \cdot 10^{-6}$ mbar.

It was observed that the surface roughness of the coatings varies **as** a function of the **pre-heating** and etching time. The substrate temperature **shows** an almost linear proportionality to the pre-heating time up to a temperature of **about** 500° C. The **electron** bombardment of the substrate during the **pre-heating** procedure has " any influence on the substrate **roughness**. **However**, when the substrate was pre-heated, the final values of the substrate roughness were higher than those obtained for the same etching conditions but without previous substrate **pre-heating**. This **leads** to the conclusion, that the substrate temperature has an **influence** on the mobility of **the** surface atoms increasing the **sputtering** (etching) rate with increasing temperature.

The optimal **value** of the substrate roughness to achieve the best mechanical properties is a mean value of 0,09 μm **Rmz**.

3.3. OPTIMIZATION OF THE TARGET CHEMICAL COMPOSITION

The influence of the element nitrogen and of the substrate bias were studied when depositing films from a W-Ti target with 10 , 20 and 30 weight % titanium content.

The study of thin films deposited from the target with 10 weight % titanium showed that the substrate bias voltage during film deposition influences the properties of the W-Ti-N films. The increase of the substrate bias gives rise to dense films and decreases the nitrogen atomic content in the film. Concerning the mechanical properties, small variations were detected when changing the substrate bias.

The element nitrogen is very important. The morphology of the films is typically columnar not depending on the nitrogen flow rate. The film structures ranged from the tungsten phase up to, tungsten/titanium nitride phases. Increasing the nitrogen content of the film, increases as well its compactness. The conditions corresponding to the transition between structures without and with formation of nitrides present the best compromises between hardness and adhesion values.

Similar studies were carried out using reactive gas CH_4 and both CH_4 and N_2 . Coatings containing carbon had higher hardness (4000 Vickers) but lower scratch-test critical loads.

The study of the films deposited from the target with 20 weight % titanium showed that the nitrogen content of these films is higher than before, for the same N_2/Ar flow rate. This is due to the higher reactivity of titanium towards nitrogen in comparison with tungsten. The results of the scratch-test show lower values for the cohesive and adhesive critical loads, as well as the hardness of the films (3200 Vickers).

Similarity as before, the study of the films deposited from the target with 30 weight % titanium showed that the increase of the titanium content in the target lead to a decrease of the values for the film hardness (2200 Vickers) and for the scratch-test critical loads.

The morphology of the films is similar with those deposited from targets with lower titanium content and the nitride phase could be as well detected for values over 25 % nitrogen content.

Concerning the deposition conditions it was confirmed that the deposition with the ion gun switch-on, this means with increased plasma ionisation, leads to better film properties.

Under consideration of the results obtained with the different W-Ti targets and once the user demands for **TiAlN** coatings were growing, **the** influence of the element **aluminium** in the target chemical composition was studied. For this purpose a sintered target with **W-Ti-Al** (75-20-5) weight % was used to deposit films on high speed steel and cemented carbide tools.

For this study only **N₂** was used as **reactive** gas. The hardness achieved **values** up to 2400 **Vickers**, the scratch-test critical **loads** obtained were excellent and no signs of adhesive failure were detected. The deposition conditions selected for coating the cutting tools gave rise to compact **films** presenting **the** nitride phase.

Once the target materials used -in **this** project are very expensive in their production methods, tests were also carried out with a **Ti-Cr** (50/50%) target produced by **means** of vacuum **plasma** spraying. The study was limited to the **analysis** of the influence of the target production process on the deposition conditions and chemical composition of the deposited films.

During the deposition tests any plasma instabilities were observed on the target surface. Different **N₂/Ar** flow rates were used. The results concerning the **chemical composition** show that the plasma spraying process is an alternative to the **sintering** production method.

3.4. COATING CHARACTERIZATION

The chemical composition of the coating **depend** not only on the percentage of the respective elements 'involved in the deposition process, but **also** on other technological parameters, as the bias voltage; deposition temperature, **total pressure** in the vacuum chamber and deposition rate.

Comparing the results of the cutting tests with the values obtained for film hardness and scratch-test critical loads any relationship could be established.

The study of the wear **behaviour** of those coatings carried out with the pin-on-disc equipment can be resumed as follows:

- the high temperature wear resistance is "directly linked to the cutting tool endurance. life. The best results should correspond to the lower average depth of the wear scar
- The high temperature friction coefficient should be as **low** as possible, average value and stability
- The homogeneity of the wear scar at the end of the friction test

Some coatings **could** be optimized to **fullfill** the three previous criteria.

"The cutting tests under real conditions **lead** to results, which should be compared with those of the theoretical studies., Unfortunately any relationship was found, **only** one deposition test with a good high temperature friction coefficient achieved gut results.

The results of the fretting experiments **seem to** have a better relationship to the cutting tests under **real conditions**. The coatings with lower friction coefficient had the best results deposited on cemented carbide **mills** 'and working without lubricant (air **cooling**). The coated high speed steel taps did not **show** this result with evidence.

3.5. **CHARACTERIZATION** OF COATINGS DEPOSITED BY INDUSTRIAL PROCESS

The influence of the sample hardness on the measured value for the coating depends extremely on coating thickness and on the substrate hardness. This influence was **studied** for stainless steel, high speed steel and cemented carbide.

The study of the surface roughness was **carried** out for different initial values. The coating induces a lower surface roughness for the samples with higher roughness values. On the opposite, very smooth surfaces get higher roughness, when coated. **This** depends on the type of coating, as well as on the film deposition **rate**. A decrease of **the** deposition rate favors the film **growth** mechanisms and increases the coating quality.

The **morphology** of W-Ti-N coatings deposited when increasing substrate bias and comparative an industrial **SILVER-TiN** coating with high nitrogen atomic content in the film **show that the** film growth structure for **SILVER-TiN** is not evident, **but for the W-Ti-N** film a typical columnar growth can be observed.

Variations of the, deposition **parameters** in the industrial equipment were carried **out** for comparative **purposes**. The deposition parameters. were changed according to the working conditions, once the influence of the deposition rate **and** of the **Argon** partial pressure should be studied. The nitrogen **flow** rate was also changed when depositing **SILVER-TiN** coatings.

The results of these comparative studies **showed** that:

1) When changing the deposition rate from 2,0 up to 3,5 **nm/sec** or the Argon partial pressure from 1,3 Up to $2,2 \times 10^{-3}$ **mbar**, any influence of the deposition rate **could be detected**, as well as of the Argon partial pressure, on the hardness and **on** the surface roughness of the **GOLD-TiN** coating

2) **When** changing the deposition rate from 1,2 Up to 11,0 **nm/sec** the hardness of the **SILVER-TiN** coating increases. At higher deposition rates there is a formation of hot spots, on the target surface, due specially to **unpurities** of the **vaccum atmosphere**.

3) The deposition of **TiCN** was **done** using **CH₄** and **C₂H₂**. When increasing the Argon partial **pressure**, the formation of **arcs** on the target surface can be avoided. For a pressure above $2,0 \times 10^{-3}$ mbar the plasma can be kept **stable during a long time** (film thickness up to 5 microns). **When** decreasing the **deposition** rate, the plasma **gets** more stable and the hardness of the, coating increases.

3.6. DEVELOPMENT OF A **MULTILAYER** COATING SYSTEM

The development of a new coating based on a typical **multilayer** system similar to TiCN (titanium **carbonitride**) was carried out, once the results obtained with W-C/N-M coatings were not satisfying.

The influence of the most important **technological** parameters on the coating properties was studied, as **well** as the chemical composition and the structure of the different layers.

The chemical composition of the functional coating was **controled** by means of the **reactive** gas **flow**, which influence on the **microhardness** of the **films** was studied.

The influence' of the target load (**deposition** rate) on the **microhardness** is 'very significant for values under 20 W/cmZ'. Above this **limit**, the **Vickers** hardness keeps its **value** constant (2800 NV).

The substrate bias has any influence on the film growth, on the surface' roughness and on the adherence of the coating for values above 80 and up to 150 Volt.

3.7. DEVELOPMENT OF **NEW CHARACTERIZATION METHODS**

Two tests were developed to try to get more information about film stresses and film strength, as well as to characterize the adhesion of the coating to the substrate:

CST - CRACK STRENGTH TEST

This test can be described as a **Bend-Break-Test** of, brittle materials. For this purpose, a soft substrate material with low hardness is coated with a film of specified thickness. The surface is loaded by the diamond indenter of a **Vickers microhardness** measurement equipment. With increasing load, a limit value is reached which induces the film to break through into the substrate.

The development of the CST test and the definition of the test conditions were realized using aluminium alloy samples, as, substrate material, and multiple layer coatings were deposited with variable , thickness up to 50 μm for **Silver-TiN**.

SST - SOFT SCRATCH TEST

Scratch testers use a diamond indenter and are used to measure a theoretical adhesion (the critical load L_c) quality of thin films. Any kind of relation can be established between the measured critical load values and the results of the lifetime tests with cutting tools, as well as any kind of relation can be established between critical load and the measured hardness values.

The coating structure and hardness are important factors; which have a great influence on the critical load values obtained with the diamond scratch tester.

The method proposed to test the adhesion quality of thin films is very similar, but instead of a diamond indenter here a cemented carbide indenter is used.

The study of the working conditions when using the SST equipment was done, using high speed steel and cemented carbide substrates. The coating thickness was chosen at three levels, depositing approx. 3, 5 and 7 μm for single and multiple layer coatings.

The SST load range was defined at stages 0, 1, 2 and 3 (equivalent to 250, 500", 750 and 1000g). The relative movement of the cemented carbide indenter is carried out in two ways: in one way to obtain a surface pressure under an angle of 75° and in the opposite way to obtain shear forces under an angle of 15°.

3.8. WEAR CHARACTERIZATION AND GEOMETRY DEVELOPMENT

The wear **behaviour** of the cutting tools shows, as expected, that the critical regions are the cutting edges for both cemented carbide end mills and HSS taps. The **friction surfaces** of the cutting tools, which are in contact with the worked material **during** service, are **also** critical regions, as the 'free angle side of the cutting edge.

The most significant aspects to be considered for the geometry definition are certainly the creation of stable cutting edges, **the** optimization of the surface roughness and the increase of the substrate material strength. The coating gives a **higher** protection to the cutting edge, increases the material **strength** of the substrate **surface** and decreases the friction **coefficient**.

To calculate the exact profile of cemented carbide cutting tools to be developed or optimized, a software **programme** was used, which **allows** to calculate the **optimal** profile for the tool, to **simulate** a cutting tool 'and to design the profile" 'for the grinding wheel, with which the designed **tool will be produced. Different types** of drills were tested coated with standard coatings. **This** development showed the influence of the coating properties on the tool geometry.

The results-of the cutting tests with different PVD coatings and special surface treatments of high speed steel taps show the dependency of the tool wear behaviour from **those** parameters.

Other tests run to determine the torque by thread forming using taps from type **FORMEX** with different **poligon** forms and with an **oxinitriding** surface treatment. The results **have** shown that "with a flat **poligon** form the torque is higher than that of a pointed form. The lifetime for both k'inds of **poligons** was similar.

3.90 ANALYSIS OF THE EFFECT OF SUPPLEMENTARY COATING THICKNESS

Certainly there is a difference between **HSS** taps or **formers** on one side and cemented carbide **drills** and end **mills** on the other side.

With increasing coating thickness, the lifetime of the cutting **tools** increases proportionally. For any kind of tool there a **threshold** for the coating thickness, which should be estimated.

HSS taps are sensible to variations of the coating thickness for "films with higher roughness, but not as much as-by formers.

The development of heat on the contact **surface** during service leads to the disruption of the lubricant **film**. Under **this** working conditions, the properties of the coating can change, as well as the structure of the substrate material. The adherence of the **coating** to the substrate can be lost.

Cemented carbide **tools** need thicker coatings for better protection of the cutting edges. The limits for the coating thickness are different for drills and for end mills.

Drills can be coated with a film thickness higher than 3 μm and the lifetime **still** increases, depending on the worked material.

The common material used for cutting **tests** was heat treatable **tool** steel, for which the coating thickness should achieve values up to 4,0 microns. For working general structural steel a coating thickness up to 5 microns can be used with very good lifetime results. With **increasing strength** of the worked material the coating thickness must be decreased.

3.10. CUTTING TOOLS. WITH **NEW** GEOMETRIES' AND **NEW** COATINGS

Cemented carbide for **tool** production was **obtained** from different producers. The specifications were done corresponding **to the** type of tool to be tested considering the worked **material**.

A new cemented carbide quality for tool production was optimized and the study of the wear **behaviour** of coated tools was carried out.

The new cemented carbide type is **CERMETS**, which has other chemical and mechanical properties as usual standard materials, **as** better wear resistance, higher chemical stability, higher resistance against temperature differences and lower bend **strenght**.

With the purpose to use **CERMETS** for **tool** production it was necessary to adjust the tool geometry to the mechanical properties of that material. Tests of **mill cutters** with **two,** three, four and six flutes were carried out, leading to better lifetime of the tool **compared** with conventional cemented carbide.

New geometries for standard tools were used for further development. These tools were coated and **tested**, in such a way that the geometrical limits could be defined for those tools.

Coated tools with **new** geometries were produced and tested uncoated and coated with standard coatings, **as well** as with the new developed **multilayer** coating. Tests were carried out with coated cemented carbide drills and HSS taps and **formers**.

The optimization **of** the coating **properties** lead to deposition tests with standard end **mills** and new **developed** drills, as well as **for** new designed taps and **formers**. Mainly, an interlayer at the beginning of the deposition process was **introduced** to increase the adherence of the coating to the substrate. Also switching on the ion gun during the deposition increases the **quality** of the coating.

The, best results were achieved by the **multilayer** coated tools for emulsion coolant and by W-C/N-Me coated tools for air coolant.

Working with coated HSS taps and **formers**, low torque values and high lifetime of the W-C/N-Me coated taps **could** be achieved.

The coating thickness distribution **depends** on the deposition conditions, which can be optimized for that purpose, but the most important aspect is certainly the tool geometry.

Considering the tool geometry and the functional surfaces, where the wear is more significant, it is not possible to influence the coating thickness distribution **by** means of changing the tool geometry.

4. RESULTS AND CONCLUSIONS

The results achieved with the new **developed W-C/N-Me** coatings showed a **continuous** positive development considering the life-time of the cutting tools. The optimization of the target chemical composition and of the **respective** deposition **conditions** lead to very significant results, specially those related with the cemented carbide end mills. These were tested **under** real cutting conditions and showed different wear **behaviour** when **using** lubricant or only press air as coolant..

Coatings containing tungsten seem to have better high temperature wear resistance, also compared with some standard coatings. Under dry cutting conditions, the life-time could be increased up to 200 %, **also** when using the 'optimized **SILVER-TiN** and **MULTILAYER** coatings.

The best results were **achieved** with coatings deposited from a **W(70)-Ti(30)** target. Nitride coatings **achieved** the best results under dry cutting conditions and **carbonitride** coatings using emulsion as coolant and' lubricant.

Once more could be confirmed that with increasing titanium content the quality of the coating, increased **similarly**. On the other hand, the introduction of **aluminium** in the chemical composition of the target leads to a decrease of the coating quality.

The results achieved with **coated HSS taps** and **formers** were not very promising. The higher life-time of the tools was achieved with coatings deposited also from the **W(70)-Ti(30)** target. With nitride and **carbonitride** coatings some good results **were** achieved. The life-time was lower than that of the standard coatings and achieved not more than 75 % of the reference values.

For high speed steel taps the cutting forces can be reduced. Resuming the results of the tests, means the surface treatments the clamp friction and **tool** wear can be reduced and the tap time life increased.

The quality of the development **departments, concerning the** characterization of hard coatings during service could be increased. Many lifetime tests were carried out with **cutting** tools, to create the standard basic data for industrial applications and for further developments of coatings.

The development of new characterization **methodes** for thin films was very useful and the results **show** very **interesting** relations to practical applications. The quantification of these parameters gave new impulses to the project. The pin-on-disc **and** fretting tests, as well as the crack strength and the soft scratch tests, can be used more often in the future.

The development of new tool geometries **lead** to better results of the lifetime with standard coatings. For these purposes a new **multilayer** coating was developed **and** deposited on cemented carbide end mills and drills, which can be commercialized.

The development of W-C/N-Me coatings lead to the optimization of the chemical composition of the target. **The** films **deposited** from the target **W,Ti** have very good adhesion and cohesion **properties**, high hardness **and** **low** friction coefficient values.

With the new **multilayer** coating **following** advantages **could** be achieved:

- higher strength than the other coatings, **which** allows to use it "for cutting **tools** working under interrupted **cutting** conditions
- higher temperature resistance **than** the **standard** **Gold-TiN** coating, i.e. higher cutting speed and feed rate are possible
- higher abrasive wear resistance than the **standard** **TiAlN** coating .
- lower affinity to titanium, **nickel** or brass,